Optimization of electrically tunable VCSEL with intracavity nematic liquid crystal

Carlos Belmonte,1 Leszek Frasunkiewicz,1 Tomasz Czyszczanowski,2 Hugo Thielen,1 Jeroen Beeckman,3,4 Kristiaan Neyts,3,4 and Krassimir Panajotov1,5,*

1B-Phot., Vrije Universiteit Brussel Pleinlaan 2, 1050 Brussel Belgium
2Institute of Physics, Lodz University of Technology, Lodz 93-005, Poland
3Department of Electronics and Information Systems, Ghent University, Ghent 9000, Belgium
4Center of Nano and Biophotonics, Ghent University, Ghent 9000, Belgium
5Institute of Solid State Physics, 72 Tzarigradsko Chaussee Blvd., 1784 Sofia, Bulgaria
*kpanajot@b-phot.org

Abstract: We optimize the wavelength tuning range of a Vertical-Cavity Surface-Emitting Laser with an intracavity layer of nematic Liquid Crystal (LC-VCSEL) lasing around 1.3 μm. The tunability is obtained by applying voltage to the liquid crystal layer, which essentially is to vary the refractive index from the extraordinary to the ordinary. We achieve 71.6 nm continuous tuning (without mode hopping) with liquid crystal thickness of about 3.2 μm. We investigate the impact of ambient temperature on the LC-VCSEL tuning range and show that mode-hop tuning can be achieved in the temperature range from –10°C to 50°C where the LC is in nematic phase.

© 2015 Optical Society of America

OCIS codes: (140.3600) Lasers, tunable; (140.7260) Vertical cavity surface emitting lasers; (160.3710) Liquid crystals.

References and links


#234966 - $15.00 USD

Received 19 Feb 2015; revised 17 Apr 2015; accepted 6 May 2015; published 5 Jun 2015

© 2015 OSA
1. Introduction

Tunable semiconductor lasers operating in the wavelength region around 1310 nm and 1550 nm are of great interest for various applications, such as biological and gas sensing [1, 2], spectroscopy [3], tomography [4] or telecommunications [5–8]. Many groups have demonstrated wavelength tuning of electrical or optically pumped VCSEL combined with Micro-Electro-Mechanical-System (MEMS) technology, using a moving membrane like a mirror to change the optical cavity length and hence provide wavelength tuning. MEMS movable reflector are typically cantilever or membrane structures using high contrast gratings or DBRs and are actuated by electrostatic, electrothermal or piezo-electric forces.

MEMS-VCSEL, in which the top DBR comprises a micromachined cantilever (c-VCSEL), was first demonstrated in 1995 in [9]. Wavelength tuning range (TR) of 15 nm was achieved for a voltage of 5.7 V. In 1999, a tunable 1.55 µm VCSEL with a 50 nm TR was developed [10]. The device top membrane with a curved mirror is pulled down by electrostatic force, when applying voltage from 0 to 39 V between the top membrane and the bottom mirror. In 2002, a wafer-fused optically pumped tunable VCSEL with output power up to 1 mW at 1.55-µm and 38 nm TR for a voltage change of 4 V was reported [11]. In 2004, the same group achieved an output power of 2 mW reducing the TR to 32 nm for a voltage below 4 V [12]. TR is further increased to 150 nm in optically pumped MEMS-VCSEL around 1.3 µm in 2012 [13].

For the first time, an electrically pumped tunable MEMS-VCSEL with a TR of 40 nm and a maximum output power of 100 µW was developed in 2004 [14]. The VCSEL is based on a two-chip concept, where the movable mirror membrane is fabricated on a separate chip, avoiding compromise between MEMS and VCSEL designs. Using a similar device, the same group improved the output power up to 1.7 mW by reducing the top mirror reflectivity, but reduced the TR till 28 nm [15]. The TR is significantly increased to 60 nm in 2006 [15] and to 76 nm in 2009 [16] using an antireflection coatings. The upper MEMS mirror is a SiO2-SiN concave DBR which can be actuated electrothermally. The maximum output power measured is 1.31 mW. A high performance electrically pumped single-mode MEMS VCSEL with a TR of 102 nm with a maximum output power of 3.2 mW was developed in 2011 [17]. The technology used is based on low temperature plasma enhanced chemical vapor deposition without wafer-bonding or wafer-gluing and is not restricted to 1.55 µm only. The SiO2-SiN2 based movable top DBR is a membrane, which is suspended on four flexible beams. When the current flows through the metallization of the top mirror membrane, the beams of the membrane are expanded, increasing the air-gap cavity length. The largest TR of 140 nm for electrically pumped MEMS-VCSEL was reported in 2014 [18]. The tunable VCSEL is based on the same structure as in [17] however, with high refractive index contrast SiO2/SiC layers movable DBR that broadens the spectral width of the reflectivity and increases the TR.

Despite the excellent and large TR, MEMS tunable VCSELs suffer from a rather complex technological process, and the separate MEMS are sensitive to mechanical vibrations. Another way to obtain wavelength tuning in VCSELs is to change its refractive index, using LC as an electro-optic material located in the cavity, forming a device without any movable part. LC-VCSELs have many advantages, such as simpler technological process, insensitivity to mechanical disturbances, small tuning response time and high reliability. A nonmechanical tunable VCSEL with a nematic LC using optical pumping was first demonstrated in 2006 [19]. The TR was 10 nm with a tuning response time of 30 µs applying a voltage of 150 V. The
structure is composed of 7 InGaAs/InGaAsP quantum wells, InP/InGaAsP bottom DBR and SiO₂/TiO₂ top DBR, grown on InP substrate. The same group presented in 2011 [20] a tunable VCSEL with a nematic LC in the 1.5 μm wavelength regime under optical pumping, with a TR of 33 nm with less than 3 V applied voltage. The structure is composed of 8 InGaAs/InGaAsP quantum wells, amorphous-Si/amorphous-SiN bottom DBR and SiO₂/TiO₂ top DBR. In 2011, an optically pumped 1.55 μm emitting tunable VCSEL using intracavity nematic LC (BL036), achieved a TR of 34 nm for a voltage change of 2.4 V [21].

Recently, we have developed technology for integration of a VCSEL chip into an LC cell [22]. Based on this technology we have shown that coupled-cavity LC-VCSEL device can be efficiently used for polarization control and polarization switching by changing the voltage applied to the LC [23] thus confirming the theoretical results of [24]. Furthermore, with a chiral LC such LC-VCSEL generates circularly rather than linearly polarized light with lower threshold current and enhanced degree of polarization [25, 26].

Because of these impressive achievements, question arises if the TR of intracavity LC-VCSEL can be further increased, especially for structures that allow for electrical pumping. We answer this question here, by carrying out an optimization of an LC-VCSEL lasing around 1.31 μm and achieve a TR of 71.6 nm. Furthermore, we investigate the impact of temperature on the TR and show that mode-hop free TR can be maintained from −10°C to 50°C for LC thickness of 2.7 μm on the expense of decreasing the TR from 77.2 nm at −10°C to 38.2 nm at 50°C.

2. Device structure

In Fig. 1 a schematic cross section of the tunable LC-VCSEL is shown, with the LC placed in-between a Half VCSEL (bottom DBR and Active Region) and a top DBR.

Fig. 1. Schematic of the cross section of a tunable LC-VCSEL with intracavity nematic LC. Detailed description of the structure with labels denoted is given in Table 1.

Our structure is based on [27], where a wafer-fusion VCSEL has been optimized for low threshold current and wide stop-band of more than 100 nm. The bottom DBR consists of 35 pairs of nid GaAs/Al₀.₉Ga₀.₁As. The bottom DBR is wafer-fused to a 5/2λ cavity grown on an InP substrate. The active region consists of six compressively strained AlGaInAs QWs with seven tensile strained barriers of AlGaInAs. The p-doped AlInAs layer acts as a current blocking layer and is followed by a buried highly doped P+ N+ tunnel junction. On top of the N-InP spacer we place the LC layer sandwiched between two alignment layers of azo dye SD1 [28]. The top DBR consists of N_{top} = 25 pairs of nid-GaAs/Al₀.₉Ga₀.₁As and 1 pair of n-doped (N = 5·10¹⁵ cm⁻³) GaAs/Al₀.₉Ga₀.₁As. We also study the cases with N_{top} = 20 and N_{top} = 16.
Finally, two intracavity highly doped contact layers achieve a proper electrical injection. The doped layer in the top DBR acts as a third intracavity contact, which is used to apply a voltage to the LC. The detailed description of the LC-VCSEL structure is presented in Table 1.

Table 1. Detailed structure of the LC-VCSEL.

<table>
<thead>
<tr>
<th>Material</th>
<th>Doping ([cm^{-3}])</th>
<th>([\text{nm}])</th>
<th>([n]_e, n_t)</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>GaAs</td>
<td>nid</td>
<td>96</td>
<td>3.41 - i10^{-4}</td>
<td>Top DBR</td>
</tr>
<tr>
<td>(Al_{0.9}Ga_{0.1}As)</td>
<td>nid</td>
<td>109.9</td>
<td>2.98 - i10^{-4}</td>
<td>Top DBR</td>
</tr>
<tr>
<td>GaAs</td>
<td>nid</td>
<td>96</td>
<td>3.41 - i10^{-4}</td>
<td>Top DBR</td>
</tr>
<tr>
<td>(Al_{0.9}Ga_{0.1}As)</td>
<td>(N = 5 \cdot 10^{18})</td>
<td>109.9</td>
<td>2.99 - i0.00016</td>
<td>Cathode Contact</td>
</tr>
<tr>
<td>GaAs</td>
<td>(N = 5 \cdot 10^{18})</td>
<td>96</td>
<td>3.41 - i0.00024</td>
<td>Cathode Contact</td>
</tr>
<tr>
<td>SD1</td>
<td>nid</td>
<td>2</td>
<td>3.2</td>
<td>Alignment Layer</td>
</tr>
<tr>
<td>Liquid Crystal</td>
<td>nid (L (LC))</td>
<td>(n_e, n_t)</td>
<td></td>
<td>Liquid crystal</td>
</tr>
<tr>
<td>SD1</td>
<td>nid</td>
<td>2</td>
<td>3.2</td>
<td>Alignment Layer</td>
</tr>
<tr>
<td>InP</td>
<td>(N = 10^{18})</td>
<td>197.5</td>
<td>3.2 - i10^{-5}</td>
<td>(9)</td>
</tr>
<tr>
<td>GaInPAs</td>
<td>(N = 5 \cdot 10^{18})</td>
<td>15</td>
<td>3.4 - i0.16</td>
<td>Anode Contact</td>
</tr>
<tr>
<td>InP</td>
<td>(N = 10^{18})</td>
<td>182</td>
<td>3.2 - i10^{-5}</td>
<td>(8)</td>
</tr>
<tr>
<td>InP</td>
<td>(N = 10^{18})</td>
<td>30</td>
<td>3.2 - i10^{-5}</td>
<td>(7)</td>
</tr>
<tr>
<td>AlGaInAs</td>
<td>(N = 5 \cdot 10^{19})</td>
<td>15</td>
<td>3.4 - i0.006</td>
<td>(6)</td>
</tr>
<tr>
<td>AlGaInAs</td>
<td>(P = 5 \cdot 10^{19})</td>
<td>15</td>
<td>3.4 - i0.006</td>
<td>(5)</td>
</tr>
<tr>
<td>AlInAs</td>
<td>(P = 2 \cdot 10^{18})</td>
<td>40</td>
<td>3.25 - i10^{-3}</td>
<td>(4)</td>
</tr>
<tr>
<td>6</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>AlGaInAs</td>
<td>nid</td>
<td>6.7</td>
<td>3.3</td>
<td>Barrier</td>
</tr>
<tr>
<td>AlGaInAs</td>
<td>nid</td>
<td>6</td>
<td>3.6</td>
<td>Well</td>
</tr>
<tr>
<td>AlGaInAs</td>
<td>nid</td>
<td>6.7</td>
<td>3.3</td>
<td>Barrier</td>
</tr>
<tr>
<td>InP</td>
<td>(N = 1.5 \cdot 10^{18})</td>
<td>20</td>
<td>3.2 - i10^{-10}</td>
<td>(3)</td>
</tr>
<tr>
<td>InP</td>
<td>(N = 5 \cdot 10^{18})</td>
<td>27.7</td>
<td>3.2 - 2.4\cdot i10^{-5}</td>
<td>(2)</td>
</tr>
<tr>
<td>GaInPAs</td>
<td>(N = 5 \cdot 10^{18})</td>
<td>15</td>
<td>3.4 - i0.16</td>
<td>Cathode Contact</td>
</tr>
<tr>
<td>InP</td>
<td>(N = 10^{18})</td>
<td>402.5</td>
<td>3.2 - i10^{-3}</td>
<td>(1)</td>
</tr>
<tr>
<td>35</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>GaAs</td>
<td>nid</td>
<td>96</td>
<td>3.41 - i10^{-4}</td>
<td>Bottom DBR</td>
</tr>
<tr>
<td>(Al_{0.9}Ga_{0.1}As)</td>
<td>nid</td>
<td>109.9</td>
<td>2.98 - i10^{-4}</td>
<td>Bottom DBR</td>
</tr>
<tr>
<td>GaAs</td>
<td>nid (\text{inf})</td>
<td></td>
<td>3.41 - i10^{-4}</td>
<td>Substrate</td>
</tr>
</tbody>
</table>

The current is uniformly distributed thanks to N-doped InP layers (1) and (2) before injection into the cavity starting with the nid InP layer (3). The layers (4) and (7) (P-AlInAs and N-InP, respectively) are spacers to adjust the tunnel junction. A uniform current injection is necessary for avoiding any filamentation of the lasing mode, which is why the current injected into the tunnel junction is spread by the N-doped spreading layers (8) and (9). Layers (1) and (9) are much thicker than the rest of the layers and are used for fine tuning the cavity thickness for the emission wavelength. In our device the tunnel junction consists of two AlGaInAs layers of 15 nm; the first one is N-type doped \((N = 5 \cdot 10^{19} \text{ cm}^{-3})\) and the second is P-type doped \((P = 5 \cdot 10^{19} \text{ cm}^{-3})\). We implement a nematic E7 LC placed between the layer (9) and the top DBR. The layer of the top DBR in contact with the LC is highly-doped and it is the cathode contact to apply the voltage to the LC. Alignment layers are required on both sides of the LC to control the orientation of its molecules. When a voltage is applied to the LC, its molecules tilt from a planar to a nearly homeotropic orientation which means that the refractive index goes from the extraordinary to the ordinary, and the laser emission wavelength of the LC-VCSEL decreases.
3. Theoretical results

Our procedure of optimizing the LC-VCSEL for large TR is based on the transfer matrix method [24, 29] to find the resonant wavelengths and the corresponding threshold gains. Three different variables of our structure are varied: the LC thickness, the number of pairs in the top DBR and the transition from the extraordinary refractive index ($n_e$) to the ordinary refractive index ($n_o$) of the LC when voltage is applied. This transition will determine the tuning spectra of our LC-VCSEL. The refractive indices for light traveling along Z axis and linearly polarized along the X and Y axes are determined by [24]

\[
\begin{align*}
    n_x &= n_o, \\
    n_y &= \frac{n_o n_e}{\sqrt{n_o^2 \sin^2(\theta) + n_e^2 \cos^2(\theta)}},
\end{align*}
\]

where $\theta$ is the angle at which the molecules are aligned with respect to the z axis. We carry out the optimization procedure by performing a sweep of the LC thickness, with fixed number of DBR and refractive index of the LC, either the ordinary or the extraordinary ($n_o$ or $n_e$). Figure 2 shows the evolution of the lowest threshold gain mode and the corresponding resonance wavelength, with the thickness of the LC. The number of pairs of the top DBR is fixed to 25.

![Threshold Gain](a) ![Resonance Wavelength](b)

Fig. 2. Threshold gain (a) and resonance wavelength (b) of the lasing mode as a function of the LC thickness. The solid blue curve corresponds to the ordinary refractive index ($n_o$) and the dashed red line to the extraordinary refractive index ($n_e$). The number of pairs of the top DBR is $N_{top} = 25$.

The period of the solid blue curve for the ordinary refractive index ($n_o=1.5036$) is 440 nm and for the dashed red line for extraordinary refractive index ($n_e=1.6899$) is 387 nm, which correspond to half of the optical wavelength of $\lambda_0 = 1.31 \mu m$ ($n_o L_o \approx n_e L_e \approx \lambda_0/2$). Due to the fact that the two periods are different, there is a situation where the peaks for the $n_o$ and $n_e$ refractive indices coincide (e.g. at $L \approx 3.3 \mu m$ and L $\approx 6.6 \mu m$). This modulation is better seen in Fig. 3 where the differences between the two curves from Fig. 2 are shown. The periodicity of the envelope of the modulation in Fig. 3 corresponds to $L \approx 3.51 \mu m$, which is given approximately by $L = \lambda/(2( n_e-n_o))$. From Fig. 3 is clearly seen that the maximum mode-hop free TR of about 71.6 nm occurs when the LC thickness is around 3.2 $\mu m$. 

#234966 - $15.00 USD Received 19 Feb 2015; revised 17 Apr 2015; accepted 6 May 2015; published 5 Jun 2015 © 2015 OSA 15 Jun 2015 | Vol. 23, No. 12 | DOI:10.1364/OE.23.015706 | OPTICS EXPRESS 15711
Fig. 3. Gain difference (a) and TR (b) as a function of the LC thickness. These figures are obtained by subtracting the two curves for $n_e$ and $n_o$ in Fig. 2.

A comparison of the three threshold gains corresponding to the maximum TR as a function of the LC refractive index for different numbers of top DBR (25, 20 and 16) can be seen in Fig. 4(a). The TR as a function of the LC refractive index for the three different cases is shown in Fig. 4(b). As can be seen, the lowest threshold gain with the largest TR is achieved with $N_{top} = 25$ pairs. Quite importantly, the TR is not strongly impacted by the reflectivity of the top mirror, remaining approximately around 72 nm.

Fig. 4. Threshold gain (a) and resonance wavelength (b) as a function of LC refractive index for three different number of DBR pairs. The black curve corresponds to $N_{top} = 25$ with a LC thickness fixed to 3.2 μm and the maximum TR is 71.6 nm. The red curve corresponds to $N_{top} = 20$ with a TR of 70 nm and LC thickness of 3.18 μm. Finally the blue curve corresponds to $N_{top} = 16$ with a TR of 67.6 nm and LC thickness of 3.16 μm.

4. Temperature effects on the LC-VCSEL wavelength tuning range

In this section we study the temperature effects on the LC refractive indices and therefore, on the TR. In a homogeneous cell, the LC exhibits two refractive indices, $n_e$ and $n_o$, depending on the incident light polarization, respectively, parallel or perpendicular to the LC director. Birefringence ($\Delta n$) is the difference between these two refractive indices; i.e. $\Delta n = n_e - n_o$. 
Fig. 5. Wavelength TR comparison for different thicknesses of the intracavity LC for a range of temperatures from $-10^\circ \text{C}$ to $50^\circ \text{C}$.

We use commercial E7 LC from Merck, with high birefringence of $\Delta n = 0.1863$ at $25^\circ \text{C}$. The temperature range of nematic LC phase is between the melting temperature of $-10^\circ \text{C}$ and the clearing temperature of $60^\circ \text{C}$ [30]. To calculate the refractive indices of the LC as a function of wavelength, we use the Cauchy Eqs. (2). For LC compounds with high birefringence, like the E7, the three-band model equations are the ones that fit better the experimental results [31], namely

$$n_{e,o} \approx A_{e,o} + \frac{B_{e,o}}{\lambda^2} + \frac{C_{e,o}}{\lambda^4},$$

where $A_{e,o}$, $B_{e,o}$, and $C_{e,o}$ are the Cauchy coefficients which are constants, independent on wavelength, but dependent on the temperature. The value of the Cauchy coefficients at $25^\circ \text{C}$ are taken from [30]; $A_{e} = 1.6933$, $B_{e} = 0.0078$, $C_{e} = 0.0028$ and $A_{o} = 1.4994$, $B_{o} = 0.0070$, $C_{o} = 0.0004$. From Eq. (2), we can obtain the refractive indices of the E7 at $25^\circ \text{C}$ as $n_{e} = 1.5036$ and $n_{o} = 1.6899$. Although the range of temperatures in which the LC of E7 is in the nematic phase is from $-10^\circ \text{C}$ to $60^\circ \text{C}$, near the clearing temperature the values of the refractive indices change drastically, in nonlinear fashion. Therefore we set the range of temperatures under study from $-10^\circ \text{C}$ to $50^\circ \text{C}$, where the refractive indices have a linear dependence on temperature, characterized by the thermooptic coefficients

$$\beta_{e,o} = \frac{dn_{e,o}}{dT}$$

From [30] we know the values of the Cauchy coefficients at $45^\circ \text{C}$, i.e. $A_{e} = 1.6565$, $B_{e} = 0.0083$, $C_{e} = 0.0024$ and $A_{o} = 1.5018$, $B_{o} = 0.0068$, $C_{o} = 0.0006$. Using Eq. (2), we obtain the refractive indices for E7 at $45^\circ \text{C}$, $n_{e} = 1.5059$ and $n_{o} = 1.6621$. Knowing the refractive indices for $25^\circ \text{C}$ and $45^\circ \text{C}$, the thermooptic coefficients can be easily obtained using Eq. (3) ($\beta_{e} = -1.835 \cdot 10^{-3}$ and $\beta_{o} = 1.15 \cdot 10^{-4}$). In such way, the refractive indices for different temperatures can be calculated from:

$$n_{e,o}(T_0 + \Delta T, \lambda) = n_{e,o}(T_0, \lambda) + \beta_{e,o} \Delta T$$

From Fig. 5 it can be seen that the maximum TR occurs when the thickness of the LC is around $3.2 \mu\text{m}$. To study the temperature effect on the wavelength tuning, we take this thickness and check the TR from $-10^\circ \text{C}$ to $50^\circ \text{C}$. Figure 5 shows the TR for three different LC
thicknesses of $L_{LC} = 3.2 \mu m, 2.7 \mu m$ and $2.3 \mu m$, where we obtain a mode-hop free TR in temperature ranges of $\Delta T = 25^{\circ}C, 40^{\circ}C$ and $60^{\circ}C$, respectively. As can be seen, mode-hop free TR can be maintained from $-10^{\circ}C$ to $50^{\circ}C$ for LC thickness of $2.7 \mu m$ on the expense of decreasing the TR from $77.2 \text{ nm}$ at $-10^{\circ}C$ to $38.2 \text{ nm}$ at $50^{\circ}C$.

Fig. 6. Resonant wavelength (a), thresholds gain (b) and maximal temperature rise $\Delta T$ in the LC above the ambient temperature (c) as a function of LC refractive index obtained by self-consistent electro-thermal-optical LC-VCSEL model. The LC thickness is $L = 2.315 \mu m$ and the tunnel junction aperture radius is $R_{TJ} = 3.5 \mu m$.

Fig. 7. Temperature distribution in a vertical cross-section of the LC-VCSEL for the extraordinary LC refractive index at the threshold current of $I_{th} = 6.43 \text{ mA}$. On the left side the LC-VCSEL layered structure is shown by white lines: the LC occupies the large uniform part between $8 \mu m$ and $10 \mu m$.

In the calculation method employed so far the internal heating of the VCSEL by the injection current has not been taken into account. Question therefore arises if this heating can prevent the wavelength tuning when electro-optically changing the LC refractive index. In order to answer this question, we have carried out 3D calculation of the LC-VCSEL system that accounts self-consistently for the injection current distribution, generated temperature distribution, its impact on the gain and the resonant optical mode at the lasing threshold [32–34]. The model was already used in simulations of similar structures and revealed very good agreements with experiment [35]. Example of such calculations for LC thickness of $2.315 \mu m$ is presented in
Fig. 6, where the top panel presents the resonant wavelength, the middle panel the thresholds gain and the bottom panel the temperature rise in the LC above the ambient temperature as a function of LC refractive index. As can be seen from Fig. 6(a), the wavelength tuning properties of the LC-VCSEL are reproduced well by these self-consistent calculations revealing threshold gain change with LC refractive index (Fig. 6(b)), similar to the one in Fig. 4(a) obtained by the simple 1D optical solver. Quite importantly, the self-consistent LC-VCSEL model reveals that the temperature rise in the LC layer is only about $10^{\circ}\text{C}$ for a current of 6.43 mA (Fig. 6(c)) and can not therefore impact severely the wavelength tuning properties of LC-VCSEL system. Finally, Fig. 7 shows an example of temperature distribution in a vertical cross-section of the LC-VCSEL. In the intracavity contacted VCSEL considered here, heat is generated close to the active region and is mostly vertically transferred to the bottom DBR and the substrate and spread laterally in the semiconductor material.

5. Conclusion

An optimization has been carried out to achieve the maximum wavelength tuning range (TR) of a VCSEL lasing around 1.3 $\mu$m with an intracavity nematic LC (E7). A TR of 71.6 nm at room temperature (25°C) is obtained for a LC thickness of 3.2 $\mu$m: when the refractive index of the LC goes from the extraordinary to the ordinary the laser emission wavelength decreases from 1342.7 nm to 1271 nm. The threshold gain remains lower than 2500 $\text{cm}^{-1}$ (3200 $\text{cm}^{-1}$) in the whole TR for a top DBR with $N_{\text{top}} = 25$ (20) pairs. Decreasing the top DBR reflectivity increases the threshold gain, however it does not impact the tuning range. We have also checked the impact of the ambient temperature on the tuning range. For the E7 LC studied here, the temperature range of the nematic phase is from $-10^{\circ}\text{C}$ to 60°C. We have shown that a mode-hop free TR can be maintained from $-10^{\circ}\text{C}$ to 50°C for LC thickness of 2.7 $\mu$m on the expense of decreasing the TR from 77.2 nm at $-10^{\circ}\text{C}$ to 38.2 nm at 50°C. Finally, we ascertain our findings by a 3D calculation of the LC-VCSEL system that accounts self-consistently for the injection current distribution, generated temperature distribution, its impact on the gain and the resonant optical mode at the lasing threshold.

Acknowledgments

The authors acknowledge the financial support of FWO-Vlaanderen project G.0656.09N and the Interuniversity Attraction Poles program of the Belgian Science Policy Office, under grant IAP P7-35 photonics@be. K.P. acknowledges project DFNI-T02/18 of Bulgaria National Science Fund. H. T. and K. P. are grateful to the Methusalem foundation for financial support. This work was also supported in part by the Polish National Science Centre, Project DEC-2012/06/M/ST7/00442.